

$$3.9-5 \quad \left. \begin{array}{l} \textcircled{1} \quad C_p = C_v + \frac{TV\alpha^2}{NK_T} \\ \textcircled{2} \quad K_T = K_S + \frac{TV\alpha^2}{NC_p} \end{array} \right\} \begin{array}{l} \textcircled{1} \times K_T - \textcircled{2} \times C_p \Rightarrow \\ C_p K_T - C_v K_T = K_T C_p - K_S C_p \\ \therefore C_p / C_v = K_T / K_S \end{array}$$

$$3.9-6. \quad u = A e^{b(CV - V_0)^2} s^{4/3} e^{s/3R}$$

(a) Nernst theorem

$$\left[ T = \left( \frac{\partial u}{\partial s} \right)_v \rightarrow 0 \text{ as } s \rightarrow 0 \right]$$

Differentiate  $u$  w.r.t  $s$  at const  $v$

$$T = \left( \frac{\partial u}{\partial s} \right)_v = A e^{b(CV - V_0)^2} \left( \frac{4}{3} s^{1/3} + \frac{1}{3R} s^{4/3} \right) e^{s/3R} \rightarrow 0 \text{ as } s \rightarrow 0$$

Therefore, Nernst theorem is satisfied.  $\leftarrow$

$$(b) \quad C_v = T \left( \frac{\partial s}{\partial T} \right)_v$$

Since we already know  $T(s)$  from (a), we can get  $C_v^{-1}$  expression by differentiating  $T$  w.r.t  $s$  and divide by  $T$ .

$$\begin{aligned} \left( \frac{\partial T}{\partial s} \right)_v &= \frac{\partial}{\partial s} \left[ A e^{b(CV - V_0)^2} \left( \frac{4}{3} s^{1/3} + \frac{1}{3R} s^{4/3} \right) e^{s/3R} \right]_v \\ &= A e^{b(CV - V_0)^2} \left[ \left( \frac{4}{9} s^{-2/3} + \frac{4}{9R} s^{1/3} \right) + \left( \frac{4}{3R} s^{1/3} + \frac{1}{9R^2} s^{4/3} \right) \right] e^{s/3R} \end{aligned}$$

$$\therefore C_v^{-1} = \frac{1}{T} \left( \frac{\partial T}{\partial s} \right)_v$$

$$= \left[ \frac{\frac{4}{9} s^{-2/3} + \frac{4}{9R} s^{1/3}}{\frac{4}{3} s^{1/3} + \frac{1}{3R} s^{4/3}} + \frac{1}{3R} \right]$$

when  $T \rightarrow 0$  (i.e.  $s \rightarrow 0$  from (a))

$$C_v \sim 3s \sim T^3$$

$\hookrightarrow$  from (a) when  $s \rightarrow 0$   $T \sim s^{1/3}$

(c) when  $T \rightarrow \infty$  ( $s \rightarrow \infty$ )

From (b)

$$C_v^{-1} \sim \left[ \frac{1}{3R} s^{-1} + \frac{1}{3R} \right] \sim \frac{1}{3R}$$

$$\therefore C_v \sim 3R \sim 3Nk_B$$

Therefore the molar heat capacity  $C_v \sim 3k_B$   
at  $T \rightarrow \infty$

(d) Thermal expansion coefficient

$$\alpha = \frac{1}{v} \left( \frac{\partial v}{\partial T} \right)_p = ? \quad \text{as } p \rightarrow 0$$

$$\text{From } u = A e^{b(v-v_0)^2} s^{4/3} e^{s/3R}$$

$$-p = \left( \frac{\partial u}{\partial v} \right)_s = 2Ab(v-v_0) e^{b(v-v_0)^2} s^{4/3} e^{s/3R} = 2b(v-v_0)u$$

as  $p \rightarrow 0$   $v \rightarrow v_0$  (i.e.  $v$  becomes constant)  
as the pressure approaches to zero value.

$$\boxed{-p = 2b(v-v_0)u}$$

↳ differentiate with respect to  $T$  at constant  $p$

$$0 = 2b \left( \frac{\partial v}{\partial T} \right)_p u + 2b(v-v_0) \left( \frac{\partial u}{\partial T} \right)_p$$

$$\therefore \frac{1}{v} \left( \frac{\partial v}{\partial T} \right)_p = \frac{(v-v_0)}{uv} \left( \frac{\partial u}{\partial T} \right)_p = \frac{(v-v_0)}{uv} C_p \rightarrow 0$$

as  $p \rightarrow 0$  ( $\because v \rightarrow v_0$ )

3.9-8.

$v(T, p)$  in the vicinity of  $(T_0, p_0)$

$$dv \equiv v(T, p) - v(T_0, p_0) = \left( \frac{\partial v}{\partial T} \right)_p dT + \left( \frac{\partial v}{\partial p} \right)_T dp$$

$$= v_\alpha dT - v_{\kappa T} dp \quad dT \equiv \tau = T - T_0$$

near  
 $T = T_0$   
 $p = p_0$

$$= v_0 \alpha \tau - v_0 \kappa_T p \quad dp = p - p_0$$

$$= v_0 \tau [\alpha^0 + A_\alpha \tau + B_\alpha \tau^2 + D_\alpha p + E_\alpha p^2 + F_\alpha \tau p]$$

$$- v_0 p [\kappa^0 + A_\kappa \tau + B_\kappa \tau^2 + D_\kappa p + E_\kappa p^2 + F_\kappa \tau p]$$

$$v = v_0 + [v_0 \alpha^0 \tau - v_0 \kappa^0 p]$$

$$+ [v_0 A_\alpha \tau^2 - v_0 D_\kappa p^2 + (v_0 D_\alpha - v_0 A_\kappa) \tau p]$$

$$+ [v_0 B_\alpha \tau^3 - v_0 E_\kappa p^3 + v_0 E_\alpha \tau p^2 + v_0 F_\alpha \tau^2 p - v_0 B_\kappa \tau^2 p - v_0 F_\kappa \tau p^2]$$

~~$$= v_0 + (v_0 \alpha^0 - v_0 \kappa^0)$$~~

$$v = v_0 + \{ v_0 \alpha^0 \tau - v_0 \kappa^0 p \}$$

$$+ \{ v_0 A_\alpha \tau^2 + v_0 (D_\alpha - A_\kappa) \tau p - v_0 D_\kappa p^2 \}$$

$$+ \{ v_0 B_\alpha \tau^3 + v_0 (F_\alpha - B_\kappa) \tau^2 p + v_0 (E_\alpha - F_\kappa) \tau p^2 - v_0 E_\kappa p^3 \}$$



3.9-9

$$S(T, p_0) \quad ds = \left( \frac{\partial S}{\partial T} \right)_p dT$$

$$S(T, p_0) - S(T_0, p_0) = \frac{1}{T} C_p \tau$$

$$\therefore S(T, p_0) = S(T_0, p_0) + \frac{1}{T_0 + \tau} [C_p^0 + A_c \tau + B_c \tau^2 + D_c p_0 + E_c p_0^2 + F_c \tau p_0]$$

$\tau$  is small

$$\therefore S(T, p_0) = S(T_0, p_0) + \frac{1}{T_0} [C_p^0 + A_c \tau + B_c \tau^2 + D_c p_0 + E_c p_0^2 + F_c \tau p_0]$$

4.4.1.  $C = A + BT$ . ( $A = 8 \text{ J/K}$ ,  $B = 2 \times 10^{-2} \text{ J/K}^2$ ,  $T_{10} = 400 \text{ K}$ ,  $T_{20} = 200 \text{ K}$ )

$$\Delta U = \int_{T_{10}}^{T_f} C(T) dT + \int_{T_{20}}^{T_f} C(T) dT = 0$$

$$= \int_{T_{10}}^{T_f} (A + BT) dT + \int_{T_{20}}^{T_f} (A + BT) dT$$

$$= A(T_f - T_{10}) + \frac{1}{2} B(T_f^2 - T_{10}^2) + A(T_f - T_{20}) + \frac{1}{2} B(T_f^2 - T_{20}^2)$$

$$= 0$$

$$BT_f^2 + 2AT_f - A(T_{10} + T_{20}) - \frac{B}{2}(T_{10}^2 + T_{20}^2) = 0$$

$$T_f = \frac{-A + \sqrt{A^2 + B \left\{ A(T_{10} + T_{20}) + \frac{B}{2}(T_{10}^2 + T_{20}^2) \right\}}}{B}$$

$$\Delta S = \int_{T_{10}}^{T_f} \frac{C(T)}{T} dT + \int_{T_{20}}^{T_f} \frac{C(T)}{T} dT \approx 307 \text{ K}$$

$$\Delta S = A \log \frac{T_f}{T_{10}} + B(T_f - T_{10}) + A \log \frac{T_f}{T_{20}} + B(T_f - T_{20})$$

$$\Rightarrow \Delta U =$$

$$\Delta S =$$

4.4.2.  $C_3 = BT$  ↗  $T_{20}$ : initial temperature of the body 2.

$$\Delta U = \int_{T_f}^{T_{20}} (A+BT) dT + \int_{T_{30}}^{T_{20}} (BT) dT = 0$$

$$= A(T_{20} - T_f) + \frac{1}{2}B(T_{20}^2 - T_f^2) + \frac{1}{2}B(T_{20}^2 - T_{30}^2) = 0$$

$$\Delta S_{\text{tot}} = A \log \frac{T_{20}}{T_f} + B(T_{20} - T_f) + B(T_{20} - T_{30})$$

$$= \Delta S_2 + \Delta S_3$$

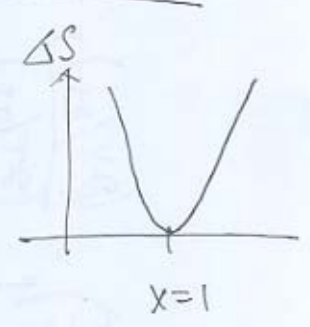
$$\sqrt{T_{30} = \left[ \frac{2A(T_{20} - T_f) + B(T_{20}^2 - T_f^2)}{B} + T_{20}^2 \right]^{1/2} =}$$

$$\Delta S_2 = A \log \frac{T_{20}}{T_f} + B(T_{20} - T_f)$$

4.4.-3

$$\Delta S = C_1 \log \left( \frac{T_f}{T_{10}} \right) + C_2 \log \left( \frac{T_f}{T_{20}} \right)$$

$$= C_1 \log \left( \frac{C_1 + C_2 X}{C_1 + C_2} \right) + C_2 \log \left( \frac{C_1/X + C_2}{C_1 + C_2} \right)$$



$$\left( \frac{\partial \Delta S}{\partial X} \right) = \frac{C_1 C_2}{C_1 + C_2 X} - \frac{\frac{C_1 C_2}{X^2}}{C_1/X + C_2} = \frac{C_1 C_2}{C_1 + C_2 X} \left( 1 - \frac{1}{X} \right)$$

$$= \frac{C_1 C_2}{C_1 + C_2 X} \left( \frac{1-X}{X} \right) \left. \begin{array}{l} > 0 \text{ for } X < 1 \\ < 0 \text{ for } X > 1 \end{array} \right\} \Delta S = 0 \text{ when } X = 1$$

$\Rightarrow \therefore \Delta S \geq 0 \text{ for } \forall X$