





# Microrheology of Soft Matters and Active Materials

### H. Daniel Ou-Yang Lehigh University

2014 Summer School on Active Systems, GIST

Introduction:

- In thermal equilibrium, mechanical fluctuations are related to the mechanical properties of the material through fluctuation-dissipation theorem (FDT).
- In an active system, noise and fluctuations can be generated by forces other than the thermal force, thus, the system does not necessarily follow the rules of FDT.
- We examine the nature of the mechanical noise in a non-equilibrium mechanical system inside a living cell to see what we can learn from it.

## Outline

- Introduction
- Experimental tools
  - Optical tweezer-based microrheology
  - Passive single particle microrheology
- Viscoelastic polymer solutions
- Microrheology in living cell
- Intracellular mechanical properties of living cells are stress dependent
- Non-thermal noise in a non-linear mechanical system

# **Mechanical Properties**



Rheology is the study of how materials deform and flow in response to externally applied force.

## **Conventional Rheometers**







# Microrheology: probes are small and often inside the materials





Active approach Oscillating tweezers Passive approach Particle tracking

**Fluctuation dissipation theorem** 

### **Optical Tweezers**

$$\Delta U = -\frac{3\varepsilon_1\varepsilon_0}{2} \left[\frac{\varepsilon_2 - \varepsilon_1}{\varepsilon_2 + 2\varepsilon_1}\right] \left|E_1\right|^2 V_2$$

Dielectric particle near the focal point of a laser

$$U(r) = -\frac{3n_1^2 V_2}{c} \left[ \frac{n_2^2 - n_1^2}{n_2^2 + 2n_1^2} \right] I_o e^{-r^2/R^2}$$



### Optical tweezers act on the trapped micro-particle like a spring

$$\vec{F} = -\Delta U = -\frac{6 r V_2 n_1}{c R^2} I_o \left(\frac{n_2^2 - n_1^2}{n_2^2 + 2 n_1^2}\right) e^{-r^2/R^2} \hat{r}$$
$$\equiv -k_{ot} r e^{-r^2/R^2} \hat{r}$$
For  $r \le 0.15 R$ , in one dimensional motions
$$F \cong -k_{ot} x$$
$$k_{ot} \approx 10 p N / \mu m = 1 \times 10^{-5} N / m$$



# Setup of optical tweezers



## **Optical Tweezers as a Micro-spring**





 $m\ddot{x}(\omega,t) = -6\pi\eta a\dot{x}(\omega,t) + k_{OT}(Ae^{i\omega t} - x(\omega,t))$ 

Valentine, UCSB

Valentine, et al., J. Phys.: Condens. Matter, 8, p. 9477–9482 (1996.).

#### **Calibration of the Force Constant of Optical Tweezers**

$$x(\omega,t) = D(\omega)e^{i(\omega t - \delta(\omega))}$$

$$D(\omega) = \frac{Ak_{OT}}{\sqrt{k_{OT}^2 + (6\pi\eta a\omega)^2}}$$

$$\delta(\omega) = \tan^{-1}\left(\frac{6\pi\eta a\omega}{k_{OT}}\right)$$

Lock-in Amplifier: how does it work?

Polystyrene particle (diameter =  $1.5 \mu m$ ) in de-ionized water, 6 mW of laser power



14.70±0.42 pN/µm

#### Why Use a Lock-In?

Suppose the signal is a 10 nV sine wave at 10 kHz. Clearly some amplification is required to bring the signal above the noise.

Now try following the amplifier with a phase-sensitive detector (PSD). The PSD can detect the signal at 10 kHz with a bandwidth as narrow as 0.01 Hz! In this case, the noise in the detection bandwidth will be 0.5  $\mu$ V (5 nV/ $\sqrt{Hz} \times \sqrt{.01}$  Hz  $\times 1000$ ), while the signal is still 10  $\mu$ V. The signal-to-noise ratio is now 20, and an accurate measurement of the signal is possible.

#### **Phase-Sensitive Detection**

Typically, an experiment is excited at a fixed frequency and the lock-in detects the response from the experiment at the reference frequency.

Signal:  $V_{sig}sin(\omega_r t + \theta_{sig})$ , where  $V_{sig}$  is the signal amplitude,  $\omega_r$  is the signal frequency, and  $\theta_{sig}$  is the signal's phase.

Reference:  $V_{L}sin(\omega_{L}t + \theta_{ref})$ .

The output of the PSD: product of two sine waves.

$$V_{psd} = V_{sig}V_{L}sin(\omega_{r} t + \theta_{sig}) sin(\omega_{L} t + \theta_{ref})$$
$$= \frac{1}{2} V_{sig}V_{L} \{ cos[(\omega_{r} - \omega_{L}) t + (\theta_{sig} - \theta_{ref})] - cos[(\omega_{r} + \omega_{L}) t + (\theta_{sig} + \theta_{ref}] \}$$

The PSD output is two AC signals, one at the difference frequency ( $\omega_r - \omega_L$ ) and the other at the sum frequency ( $\omega_r + \omega_L$ ).

If the PSD output is passed through a low pass filter, the AC signals are removed. What will be left? In the general case, nothing.

However, if  $\omega_r$  equals  $\omega_L$ , the difference frequency component will be a DC signal. In this case, the filtered PSD output will be:

$$V_{psd} = \frac{1}{2}V_{sig}V_{L}\cos(\theta_{sig} - \theta_{ref})$$

This is a very nice signal; it is a DC signal proportional to the signal.

### Normalized Displacement D/A, and phase shift δ vs. frequency 1.6 µm silica particle in water.



•: 48mW laser power at the optical trap,  $k_{OT} = 0.011$  dyne/cm •: 152mW laser power at the optical trap,  $k_{OT} = 0.034$  dyne/cm



M-T Wei et al. SPIE Proc. 8458 (2012)

#### Response Function for an Oscillating Particle in a Viscoelastic Medium

$$6\pi\eta^* a\dot{x}(\omega,t) + k_{OT} x(\omega,t) = k_{OT} A e^{i\omega t}$$

$$G^{*}(\omega) = i\omega\eta^{*}(\omega) = G'(\omega) + iG''(\omega)$$
$$G'(\omega) = \frac{k_{oT}}{6\pi a} \left(\frac{A\cos\delta(\omega)}{D(\omega)} - 1\right) \quad and \quad G''(\omega) = \frac{k_{oT}}{6\pi a} \left(\frac{A\sin\delta(\omega)}{D(\omega)}\right)$$



Larry Hough, Solvay

# Two-particle active microrheology for an inhomogeneous medium



Hough et al Phys Rev E, (2002).

# Two-particle active microrheology for an inhomogeneous medium

$$G_{12}^{*}(\omega) = \frac{k_{OT}}{4\pi R} \left[ \frac{A}{x_2(\omega)} + \frac{x_1(\omega)}{x_2(\omega)} \left( \frac{x_1(\omega)}{A} - 2 \right) \right]$$

$$G_{12}'(\omega) = \frac{k_{OT}}{4\pi R} \left[ \frac{A\cos\delta_2(\omega)}{D_2(\omega)} + \frac{D_1^2(\omega)\cos(\delta_2(\omega) - 2\delta_1(\omega))}{AD_2(\omega)} - \frac{2D_1(\omega)\cos(\delta_2(\omega) - \delta_1(\omega))}{D_2(\omega)} \right]$$

$$G_{12}''(\omega) = \frac{k_{OT}}{4\pi R} \left[ \frac{A\sin\delta_2(\omega)}{D_2(\omega)} + \frac{D_1^2(\omega)\sin(\delta_2(\omega) - 2\delta_1(\omega))}{AD_2(\omega)} - \frac{2D_1(\omega)\sin(\delta_2(\omega) - \delta_1(\omega))}{D_2(\omega)} \right]$$

# Two-particle active microrheology for an inhomogeneous medium



A comparison between (a) the local storage modulus  $G'_{11}(w)$  and the nonlocal storage modulus  $G'_{12}(w)$ ; (b) the local loss modulus  $G''_{11}(w)$  and the non-local storage modulus  $G''_{12}(w)$ , at several particle-distances for a 20 *wt%* solution of PEO. In the legends in the lower right, "R" is the distance between the two probe particles and "a" is the particle radius.

Hough et al, Phys Rev E, 2006

Passive microrheology:

Use of thermal fluctuation to determine viscoelasticity

Fluctuation-dissipation theorem

$$\alpha''(\omega) = \frac{\omega}{2k_{B}T}C(\omega)$$

 $C(\omega)$  is the power spectral density of the thermal noise of a Brownian particle  $\alpha$ " is the Imaginary part of 1/G

Passive microrheology:

Use of thermal fluctuation to determine viscoelasticity

**Kramers-Kronig relation** 

$$\alpha'(\omega) = \frac{2}{\pi} P \int_0^\infty \frac{\xi \alpha''(\xi)}{\xi^2 - \omega^2} d\xi = \frac{2}{\pi} \int_0^\infty \cos(\omega t) dt \int_0^\infty \alpha''(\xi) \sin(\xi t) d\xi$$

$$G'(\omega) = \frac{1}{6\pi a} \frac{\alpha'(\omega)}{\alpha'(\omega)^2 + \alpha''(\omega)^2}$$

$$G''(\omega) = \frac{1}{6\pi a} \frac{-\alpha''(\omega)}{\alpha'(\omega)^2 + \alpha''(\omega)^2}$$

B. R. Dasgupta, et al., "Microrheology of polyethylene oxide using diffusing wave spectroscopy and single scattering," *Phys. Rev. E*, vol. 65, p. 051505, 2002.

## Microrheology of Polymer Solutions

Viscoelasticity of PEO Solutions obtained by active and passive methods





Hough et al J. Nanotechnology (1999). Latinovic, Hough et al J *Biomechanics* (2010).

Latinovic, U. Maryland

# Microrheology with intracellular and extracellular probes



### **Microrheology of Living Cells**

- (b) Data probed by anti-integrin conjugated silica particles attached to the plasma membrane.
- (c) Data probed by intracellular organelles
- The exponents of the power-law dependence of G on frequency.
- Differences in the magnitudes of the moduli from the two measurements may be caused by extensional stiffness of the plasma membrane





Wei et. al. OE 16 8594 (2008)

# Intracellular Measurements of the Cell Mechanical Properties



Maron Mengistu, U. Maryland

Frequency-dependent G' and G" of Bovin Vascular Endothelial Cells (BVEC) using endocytosed polystyrene beads as probes



# Intracellular inhomogeneity probed with 2 polystyrene beads



- Large dynamic fluctuations are intrinsic to live cells
- Spatial inhomogeneity seems to be caused by these dynamic fluctuations

Hypothesis:

- F-actin network and the associated molecular motors are responsible for the fluctuations
- Nutrient depletion
- Depolymerization of cytoskeleton protein network

### Endocytosed polystyrene beads were used to probe the effect of nutrient depletion on G' and G'' fluctuations



# Effect of cytochalasin B treatment (actin filaments depolymerized)



# Effect of nocodazole treatment on viscoelastic properties (microtubules depolymerized)



### Nutrient depletion of drug treated BAECs



### Comparison of Active and Passive Microrheology in Living Cells





Active approach Oscillating tweezers Passive approach Particle tracking

**Fluctuation-dissipation theorem** 

## Passive Microrheology

$$C(\omega) \equiv \int \langle X(t)X(0) \rangle \exp(i\omega t) dt$$

$$\alpha''(\omega) = \frac{\omega}{2k_BT}C_{eq}(\omega) \qquad : \alpha \equiv \frac{X}{F} = \frac{1}{6\pi aG}$$

# A model bioactive system composed of actin, myosin, and biotin/neutravidin cross-links

D. Mizuno et al., Science 315, 370 - 373 (2007)



Effect of filament tension on the response of the active networks (actin and myosin concentrations as in Fig 1)



D. Mizuno et al., Science 315, 370 - 373 (2007)

Stress-dependent cell stiffness: a theoretical model



Fig. 4. (A) Schematic illustration of tension development in actin filaments (red)



D. Mizuno et al., Science 315, 370 - 373 (2007)

The apparent mechanical properties in living cells are modulated by active biological forces! The dynamical fluctuation in the mechanical properties are caused by fluctuating biological forces!

 $m\ddot{x}(\omega,t) + 6\pi\eta[F_2]a\dot{x}(\omega,t) + k[F_2]x(\omega,t)$ 

$$=k_{OT}Ae^{i\omega t}$$

+F<sub>1</sub>(thermal fluctuation) +F<sub>2</sub>(active biological foces)

- Relationship of fluctuations and dynamic tension?
- Response to defined external perturbations: pump and probe experiments
- Relate biological functions to these fluctuation dynamics

Mechanical fluctuations in living cells do not follow FDT

The normalized total fluctuation noise power spectral density  $(2k_BT\alpha''/\omega)$  probed by

- (a) an endogenous endosome (more active)
- (b) an engulfed micro-particle (less active).



M-T Wei et al. SPIE Proc. 7762 (2010)

# Total fluctuation vs. thermal fluctuation power spectra densities



Intracellular stiffness of HeLa cells increases with increasing substrates stiffness











A "non-thermal force"  $< f^2 >$  can be obtained from the fluctuations spectra by PMR and the cell stiffness by AMR.

$$\langle f^2 \rangle \alpha^{*2} = C - C_{thermal} = C - \frac{2k_B T \alpha''}{\omega}$$

A. Levine, F. MacKintosh, PRL 2009

- C. Wilhelm, *PRL*, **101**, p. 028101, 2008.
- F. Gallet, D. Arcizet, P. Bohec, and A. Richert, Soft matter, 5, p. 2947, 2009
- D. Mizuno, R. Bacabac, C. Tardin, D. Head, and C. F. Schmidt, PRL 102, p. 168102, 2009
- D. Robert, T. Nguyen, F. Gallet, and C. Wilhelm Plos One, 5, p. e10046, 2010.

# Non-thermal force spectrum increases with increasing substrate rigidity



$$< f^2 > = K^2 \Delta x^2_{nonthermal}$$

Intracellular dynamic pulling stress ( $\Delta \sigma$ ) increases with increasing substrate rigidity



### Assumption:

fluctuations in intracellular differential stiffness are caused by fluctuations in intracellular stress



$$\Delta K' \equiv \Delta K'_{rms} = \frac{1}{\tau} \int_0^\tau \left( K'(t) - \left\langle K' \right\rangle \right)^2 dt \quad \text{@1Hz}$$

# Difficult to determine local stress level in cells: can one use $\Delta K' / \Delta \sigma$ to determine intracellular stress?



 $\sigma(K') = \int (1/slope) dK'$ 

M.L. Gardel et al. PNAS 103 1762 (2006)

Assumption:

Fluctuations in intracellular differential stiffness are caused by fluctuations in intracellular stress .



### $\Delta K'_{rms} / \Delta \sigma @1Hz$

increases with increasing substrate rigidity



## Integrating $\Delta K' / \Delta \sigma$ yields a master K' ( $\sigma$ ): different substrates rigidities merely shift stress level



 $K'_0$  in the absence of intracellular stress is assumed to be 5Pa, which is reported by Soft Matter **7** 3127 (2011)

### Drug treatments follow the same K' (σ): merely shift intracellular stress level



## Conclusions

- Mechanical noises in living cells do not obey the Fluctuation-Dissipation relationship
- Non-thermal force spectrum increases with increasing substrate rigidity. Force ~ frequency<sup>-2</sup>
- Fluctuations in intracellular differential stiffness are caused by fluctuations in intracellular stress
- Use  $\Delta K' / \Delta \sigma$  to determine intracellular stress
- Integrating  $\Delta K' / \Delta \sigma$  yields a master K' ( $\sigma$ ):
  - different substrates rigidities merely shift stress level
- Drug treatments follow the same K' ( $\sigma$ ):
  - Drugs merely shift intracellular stress level

#### Acknowledgments:

Bovine Vascular Endothelial Cells Experiments:

- Elizabeth Rickter (Graduate student)
- Larry Hough (Graduate student, now at Rhodia)
- Meron Mengistu (Graduate student, Biology)
- Prof. Linda Lowe-Krentz (Biology)
- Prof. Shu Chien (Whitaker Institute of Biomedical Engineering, UCSD)

Human Lung Cells Experiments:

- Steven, Ming-Tzo Wei (Gradaute Student, Bioengineering)
- Angela Zaorski (Graduate Student, Physics)
- Dr. Huseyin C. Yalcin (Mechanical Engineering)
- Dr. Jing Wang (Postdoctoral Fellow, Physics)
- Prof. Samir Ghadiali (Mechanical Engineering)
- Prof. Arthur Chiou (Yang-Ming University, Taiwan)

Funding:

Center for Optical Technologies, NSF-DMR and NSF-EEC